

A Review on Experimental Analysis for Rectangular Perforated Fin Array

I.N. Wankhede¹, N. P. Salunke²

¹PG Student, Mechanical Department, RCPIT Shirpur, Maharashtra, India

²H. O. D., Mechanical Department, RCPIT Shirpur, Maharashtra, India

*indrajitwankede3@gmail.com*¹, *sainilesh1@gmail.com*²

Abstract:-In this study, various fin geometries are referred for steady-state natural convection heat transfer. The effects of fin spacing, fin length, fin height, % of perforations, shape of perforations etc. are studied from the literature review and come up with a conclusion that the heat capacity of material should be constant for effective analysis of heat transfer rates. Hence, in this study the intention is to do the Experimental analysis for rectangular perforated fin array and development of Neural Network Model for prediction of heat transfer coefficient under different boundary conditions.

Keywords: Perforation, Fins, Steady state, Natural convection

1. INTRODUCTION

While we are working a number of the building frameworks there is a first issue of era of warmth. This created warmth can assume a part in the disappointment of the framework because of overheating. This induced warmth in a framework ought to be disseminated in the encompassing in order to hold the framework at its supported working temperatures [2]. Due to this the framework can be worked with great proficiency. In advanced electronic frameworks the wrapping thickness of circuits is much higher [2]; subsequently the issue of warming is not kidding for this situation. So as to conquer this issue, warm frameworks with agent emitters as balances are fundamental [1].

In the event that we need to fulfill the required warmth decline rate, with minimal measure of material, the blend of geometry and situating of the balances ought to be ideal. Between these varieties of geometry, rectangular blades are the most often utilized balance geometry in light of their straightforward structure, least cost and agent cooling ability [4]. There are two sorts of arrangements with affections to rectangular balance courses of action, on a level plane based vertical blades and vertically based vertical balances, have been all the more regularly utilized as a part of the applications. Be that as it may, the even introduction is not predominant in view of its tolerably second rate ability to scatter heat [2].

The simple mathematical statement of convection warmth misfortunes is given by:

$$Q_c = hA\Delta T \quad 1.1$$

As seen from Eq. (1.1), the rate of warmth decadence from the surface can be helped either by expanding the warmth exchange coefficient, h or by expanding the surface territory, A . The estimation of h can be elevated by utilizing legitimate states of constrained stream over the required surface [2]. In spite of the fact that the constrained convection is proficient, it requires an additional space for fan or blower which limits causes the improvement in

starting and support cost. Hence, constrained convection is not generally selectable. For expanding the warmth exchange, it is more best, advantageous and simple to utilize the extended surfaces [1]. To build the warmth exchange territory, it is exceptionally effective to utilize the blades over the surface. As a consequence of this the rate of warmth exchange will be increased. Be that as it may, if the quantity of balances and the dispersing between two balances are not fittingly composed then the warmth exchange rate can be lessened moreover. In spite of the fact that including more number of balances expands the surface territory, they may oppose the wind current and cause limit layer interruptions which influence the warmth exchange unsympathetically [3].

The investigational judgments identified with the warm exhibitions of rectangular blades were affirmed in writing. In this study, the enduring state characteristic convection heat exchange from a punctured vertical rectangular blade compliances jutting from a vertical base will be investigated tentatively.

2. LITERATURE REVIEW

2.1 Fin Array (Without Perforation)

The point of this writing audit is to emerge with the comprehension of the achievement and Natural convection heat exchange rate from balance exhibits up to this snippet of study. Starner and McManus [1] directed one of the underlying learns about the warmth exchange execution of rectangular balance exhibits. In their analyses, four arrangements of blade clusters were tried to investigate free convection heat exchange presentations. The balance clusters were sited with three base sorts, vertical, 45 degrees and flat. Other than the principle warmer, watch radiators were locked in to diminish side warmth misfortunes. The average warmth exchange coefficients were gained from all blade structures for all test positions. From trial information, it was found that warmth exchange rates procured from the tests with vertical clusters fell 10 to 30 percent underneath those of also separated parallel plates. For the 45-degree base position, heat exchange rates were 5 to 20 percent underneath from the qualities taken at vertical position. With

the utilization of smoke fibers, the stream structures were watched for every base position. The impact of blade stature was additionally thought and it was comprehended that balance tallness, balance dividing and base introduction influenced the warmth exchange execution expressively. Leung and Probert [2] executed another investigational study to investigate consistent state rates of warmth decline under common convective conditions from either vertically based or evenly based vertical rectangular blades. They attempted to work out the impact of balance tallness on ideal blade dividing, and subsequently, two balance lengths were locked in, specifically 10 mm and 17 mm. The tests were completed with the base of the blade cluster at either 20 °C or 40 °C over the mean temperature of the natural air in the workroom. As an aftereffect of set number of tests, it was secured that for 150 mm length of balances, the ideal blade dispersing qualities were 9.0 ± 0.5 mm to 9.5 ± 0.5 mm for the vertical balances extended outwards from the vertical base and upwards from the flat base, separately. It was likewise gathered that the change of balance tallness and base-to-surrounding temperature contrast did not disturb ideal blade separating values for the introductions considered in the study.

Leung, Probert and Shilston [3] readies an exploratory investigation of the warmth exchange rate from an arrangement of vertical rectangular blades on vertical rectangular base has been passed on. The blades were made from light aluminium compound. The spacer bars made of the same material was made to modify the division between neighbouring blades by prearranged sums. The wooden case was situated at the back of the test area to cover warm protection and radiator plate. For different blade courses of action, the analyses were controlled at base temperatures 20 °C, 40 °C, 60 °C and 80 °C over the mean temperature of surrounding air. It was firm that the ideal blade dispersing, proportionate to the greatest rate of warmth exchange, was 10 ± 1 mm. Welling and Wooldridge [4] performed another experimental study to compare actual rectangular fin experiments with those of vertical plate, enclosed duct and parallel plate data from previous studies. During the tests, guard heater plate was utilized to minimize the heat losses from the sides and rear of the set-up. Data obtained from experiments showed that with closely spaced fins, the heat transfer coefficients were smaller compared to wider fin spacing's because of boundary layer interference, which prevents air inflow. It was observed that the heat transfer coefficients of finned arrays were smaller than those of vertical plate and greater than either those of enclosed ducts or those of parallel plates. For a given base-to-ambient temperature difference, an optimum H/s (fin height to fin spacing) ratio at which heat transfer coefficient is maximum was determined from the considered fin configurations.

Harahap and McManus [5] observed the flow field of horizontally based rectangular fin arrays for natural convection heat transfer to determine average heat transfer coefficients. In the experimental unit, guard heaters and guard fins were located near the end fins to eliminate the end effects. To visualize the flow field, schlieren-

shadowgraph techniques and smoke injection were used. Several types of chimney flow were observed. For equal fin spacing and fin height, two series of rectangular fin arrays differing in length was compared. The result of comparison indicated that the array having shorter fin length (by half) had higher average heat transfer coefficient because of its effective utilization caused by single chimney flow. This result revealed that single chimney flow pattern was favourable to high rates of heat transfer. Using the average heat transfer coefficient data, the following correlations were proposed in terms of Gr, Pr, s, n, h.

$$N_{uL} = 5.22 \times 10^{-3} \left(G_{rL} P_r \frac{s \cdot n}{h} \right)^{0.570} \left(\frac{h}{L} \right)^{0.656} \left(\frac{s}{L} \right)^{0.412}$$

$$\text{for } 10^6 < G_{rL} P_r \frac{s \cdot n}{h} \leq 2.5 \times 10^7$$

$$N_{uL} = 2.787 \times 10^{-3} \left(G_{rL} P_r \frac{s \cdot n}{h} \right)^{0.745} \left(\frac{h}{L} \right)^{0.656} \left(\frac{s}{L} \right)^{0.412}$$

$$\text{for } 2.5 \times 10^7 < G_{rL} P_r \frac{s \cdot n}{h} \leq 1.5 \times 10^8$$

Where N_{uL} is the average Nusselt number based on the half fin length L, G_{rL} is the Grashoff number based on the half fin length L, n is the number of spacing in the array, s is the fin spacing and h is the fin height. All the thermo-physical properties of air are evaluated at the wall temperature.

Jones and Smith [6] performed an experimental study to predict optimum fin spacing in terms of fin height and base-to-ambient temperature difference for natural convection heat transfer from rectangular fins on horizontal surfaces has been reported by. Determination of local heat transfer coefficients were achieved by measuring local temperature gradients with interferometer. Integrating the measured local heat transfer coefficients, the average heat transfer coefficient for the array was determined. Since the determined heat transfer coefficients were for convection only and were independent of the radiation, the interferometry technique was used directly. The results have shown that fin spacing, s is primary geometric parameter that affects the heat transfer coefficient. They also compared the measured values with the limited comparable data in literature, and it was concluded that the agreement between them was satisfactory. The experimental results were correlated with the following relation:

$$N_{us} = 6.7 \times 10^{-4} \times G_{rs} P_r \times \left\{ 1 - \exp \left(\frac{0.746 \times 10^4}{G_{rs} P_r} \right)^{0.44} \right\}^{1.7} \text{ for } s < 2 \text{ in}$$

$$N_{us} = 0.54 \times (G_{rs} P_r)^{0.25} \text{ for } s > 2 \text{ in}$$

$$\frac{h_s}{h_b} = \frac{1.68}{24} \times F^3 \times \left[1 - \exp \left(\frac{-24}{1.68 F^3} \right) \right]$$

Where,

$$F = \frac{S}{H} (G_{rs} P_r)^{0.25}$$

All the required thermo physical properties of air are evaluated at the film temperature. G_{rs} is the Grashoff number based on fin spacing, P_r is the Prandtl number.

Bar-Cohen [7] analytically investigated the effect of fin thickness on free convection heat transfer performances of rectangular fin arrays. The results of analysis have shown that for each distinct combination of environmental, geometric and material constraints, an optimum fin thickness that maximizes the thermal performance of an array exists. It was suggested that in air, the optimum fin thickness value of an array can be taken approximately equal to optimum fin spacing value for the best thermal performance. Based on his analysis, the following equation which gives the fin height associated with the optimum fin spacing was proposed:

$$H_{opt}=1.7 \times \left(\frac{k}{k_{air}} \times \frac{s}{R_{as}^{0.25}} \right)^{0.5} \times t^{0.5}$$

Where R_{as} is the Rayleigh number based on fin spacing, k is the thermal conductivity of the fin material and t is the fin thickness.

Leung, Probert and Shilston [8] studied the thermal performances of rectangular fins on vertical and horizontal rectangular bases, experimentally. Experiments were performed for three different cases; horizontally based vertical fins, vertically based vertical fins and vertically based horizontal fins. Optimum fin spacing values were predicted for each case. For constant base temperatures of 40°C, 60°C and 80°C, the experiments were conducted to reveal the effect of base position on heat transfer recitals of fin arrays. For three different fin heights, namely 32 mm, 60 mm and 90 mm, and for a base temperature of 60°C, the trials were also executed. The results have shown that for vertical fins on a vertical base, fin spacing is the most effective constraint prompting the heat transfer rate. It was also determined that unlike fin spacing, the variation in fin height did not cause an operative change in heat transfer rate for vertical fins on both vertical base and horizontal base. It was clinched that between the all considered base positions vertical fins on a vertical base was the best solution for better heat transfer routine.

The impacts of changing balance length from 250 to 375 mm on the recurrence of warmth exchange and the ideal blade dispersing of vertical rectangular balances expanded from a flat or a vertical rectangular base have been considered by Leung, Probert and Shilston [9], tentatively. But blade length, other geometric parameters of various balance arrangements were kept altered for thought introductions. Trials were directed at a consistent base temperature, 40°C over that of the surrounding environment. The trial amounts for vertical base demonstrated that the expansion in blade length brought about rebate in the rate of warmth decline per unit base region from the balance exhibit. Also, the boss blade dividing ranges from 10 ± 1 mm to 11 ± 1 mm as an aftereffect of balance length increment. Then again, with level base, expansive decrease in the rate of warmth exchange per unit territory emerged when the balance length was expanded. The finest blade dispersing of on a level plane based balance cluster expanded from 11 ± 1 mm to 14 ± 1 mm as the balance length was expanded from 250 mm to 375 mm. Every one of these significances advertised that the impact of blade

length on warmth exchange execution of balance exhibits is imperative.

Leung and Probert [9] investigated assets of changing balance thickness on the rate of warmth exchange from vertical duralumin blades swelling oppositely outwards from a vertical rectangular base, tentatively with the expectation of complimentary convection conditions. The examinations were executed with five diverse blade thicknesses, in particular 1, 3, 6, 9 and 19 mm, for base temperatures of 20°C and 40°C over that of the surrounding environment, which was kept up at 20°C. It was seen that the normal ideal uniform blade thickness was 3 ± 0.5 mm, for amazing rates of warmth exchange, when the uniform partings between the neighbouring balances surpassed 20 mm and for $20 \text{ mm} \leq s \leq 50 \text{ mm}$, the ideal balance thickness diminished to some degree as either the balance detachment or the base temperature was lessened.

Yüncü and Anbar [10] achieved an experimental study of free convection heat transfer from rectangular fin arrays on a horizontal base. 15 different fin arrays and a base plate were verified. The effects of fin height, fin spacing and base-to-ambient temperature difference on heat transfer recital were inspected. It was found that the rate of convective heat transfer from the fin array mainly be contingent on these bounds. The experimental results showed that optimal fin spacing, for maximum heat transfer rate from fin array, diminished as the fin height amplified. The effect of base-to-ambient temperature on the optimal fin spacing was also discussed and it was concluded that this effect is not significant. A correlation relating the ratio of convective heat transfer rate from a fin array to that of a base plate as a function of number of fins n , fin height H and fin spacing s was estimated and proposed as:

$$\frac{Q_{fc}}{Q_{pc}} = 0.923 \times \exp \left[1.336 \times n^{-0.013n} \times \frac{H}{s} \right]$$

Yüncü and Güvenc [11] investigated the performance of rectangular fins on a vertical base in free convection heat transfer, experimentally. During experiments, the length, width and thickness of fins on arrays were kept fixed, but other parameters such as fin spacing and fin height were varied. The effects of fin height, fin spacing and base-to-ambient temperature difference on the heat transfer performance of fin arrays was observed for several heat inputs. According to the experimental results, it was deduced that fin spacing is the most important parameter in the thermal performance of fin arrays and an optimum fin spacing can be found for every fin height, for a given base-to-ambient temperature difference. This result revealed that optimum fin spacing depends on two main parameters, fin height and base-to-ambient temperature difference. The experimental results were compared with those of obtained from horizontally based fin arrays in Ref. [13]. It was concluded that for vertically based fin arrays, higher heat transfer enhancement can be achieved.

Yüncü and Mobedi [12] performed a three dimensional numerical study on natural convection heat transfer from longitudinally short horizontal rectangular fin arrays. The governing equations, momentum and energy, were solved by using a finite difference code based on

vorticity-vector potential approach. For various geometric parameters, fin length, fin height and fin spacing, flow configurations occurring in the channel of the fin arrays were analyzed. Two types of flows were defined as a result of observations. In first type flow configurations; with small fin spacing, air enters from the ends of the channel moves along the fin length and flows out at the center of the channel. On the other hand, in the second case, with large fin spacing, fresh air can also enter into the channel from the middle part since the space between two fins is sufficiently large. Then, it turns 180 degree at the base and flows up along the fin height while it moves to the central part of the channel. The effects of fin length and fin height on the heat transfer rate of horizontal fin array were also examined and it was concluded that an increase in these geometric parameters causes reduction in the rate of heat transfer from array. This is due to more boundary layer interference along the channels which lowers the amount of intake cold air in the channel.

Yüncü and Yildiz [13] investigated natural convective heat transfer from annular fins experimentally. 18 sets of annular fin arrays were tested to observe their heat transfer performances. The fin arrays were heated with several heat inputs and corresponding base and ambient temperature differences were recorded. Using the measured data, total heat transfer rates from fin configurations were evaluated. A radiation analysis was applied to estimate the rates of radiation heat transfer. Then, radiation contributions were subtracted from total heat dissipations to obtain essential convection heat transfer rates. It was concluded that the convection heat transfer rate from the fin arrays depends on fin diameter, fin spacing and base-to-ambient temperature difference. A scale analysis was also performed in order to estimate a correlation which evaluates order-of-magnitude of optimum fin spacing at a given fin diameter and base-to-ambient temperature difference. The correlation is:

$$\frac{S_{opt}}{D} = 3.38 \times R_{as}^{-0.25}$$

2.2 Fin Array (With Perforation)

Guei-Jang Huang et al. [14] planned Natural convection heat exchange rate from penetrated balance clusters has been assessed for various geometries. The hypothetical and trial study was steered to locate the finest geometric requirements in order to accomplish greatest warmth exchange from the finned surfaces. An investigational study was made to assess the impacts of blade separating, balance tallness and measure of warmth flux on blended convection heat exchange from rectangular balance exhibits. To acquire the most extreme warmth exchange ideal balance dispersing has been evaluated. Amid the trials consistent warmth flux boondocks condition was perceived and air was utilized as the working liquid. The speed of liquid entering channel was kept verging on steady (0.156win 60.16 m/s) utilizing a stream rate control valve with the goal that Reynolds number was constantly about $Re = 1500$. Experimentations were led for altered Rayleigh numbers $3 \times 10^7 < Ra^* < 8 \times 10^8$ and Richardson number $0.4 < Ri < 5$. Balance separating was changed from $S/H = 0.04$ to $S/H =$

0.018 and blade stature was differed from $H_f/H = 0.25$ to $H_f/H = 0.80$. For blended convection heat exchange, the results obtained from test study demonstrate that the ideal balance dividing which yield the most extreme warmth exchange is $S = 8-9$ mm and ideal balance separating relies on upon the estimation of Ra^*

Rigan Jain and M.M.Sahu [15] examined the relentless state common convection heat exchange from vertical trapezoidal blades augment upright from vertical rectangular base with Computational liquid elements (CFD). The impact of warmth burdens on temperature distinction in the middle of base and encompassing on the warmth exchange presentation of trapezoidal balance clusters for the ideal blade dispersing values has been measured with the assistance of reproduction models. The warmth inputs going from 25 W to 125 W has been supplied for blade arrangement, and subsequently, the base and the surrounding temperatures are measured keeping in mind the end goal to get the warmth exchange rate from balance exhibits. The outcomes are segregate with those acquired tentatively and factually for rectangular blades with same surface region, balance tip thickness and base plate extents. Yazicioğlu B.[16] examined the enduring state normal convection heat exchange from vertical rectangular blades dragging out upright from vertical rectangular base tentatively. The impacts of geometric limitations and base-to-surrounding temperature distinction on the warmth exchange presentation of balance clusters were seen and the ideal blade division qualities were resolved. Two comparative trial set-ups were locked in amid trials so as to take limits from 30 diverse balance courses of action having balance lengths of 250 mm and 340 mm. Balance thickness was maintained altered at 3 mm. Balance stature and balance separating were dotted from 5 mm to 25 mm and 5.75 mm to 85.5 mm, separately. 5 heat inputs fluctuating from 25 W to 125 W were accommodated all balance developments, and consequently, the base and the surrounding temperatures were honourable keeping in mind the end goal to assess the warmth exchange rate from balance exhibits.

Mohamad I. Al-Widyan and Amjad Al-Shaarawi [17] begin a rectangular balance having unvarying cross segment with roundabout puncturing on a surface at a consistent temperature. The punctured balance was purposeful under regular convection utilizing familiar ansys for warmth exchange expansion similar to its strong partner considering distinctive levels of Grashoff numbers and two geometric limits: as dividing between gap, sx , and opening measurement, D . It is found that, over the decisions considered, heat exchange from the penetrated balance enhanced with Grashoff number. Also, warm exchange opened up as the dispersing between gaps dwindled. Concerning the opening measurement, about all cases displayed an upsurge in warmth exchange with width barring for the instance of high Grashoff number and high dividing proportion, ϵ , where a greatest estimation of warmth exchange advancement is touched then begun to fall again with the distance across calling for further

investigation that incorporates the balance thickness. This study thinks about a solitary rectangular blade with an even warm conductivity, undeviating cross area with length L , thickness of $0.1L$, and is endlessly wide. The blade is punched with roundabout gaps along the balance length and balance width. Every puncturing (opening) has a width D and is sliced vertically through the blade's body (thickness). The segments of openings are disengaged from each other by a separation S_x in the heading upright to the blade length. In the same segment, opening are consistently scattered toward L and are incoherent by a separation $S_y=L/4$. The blade is given to a vertical surface at a relentless temperature T_s and works under common convection circumstances where the besiding liquid is required to have steady properties with a uniform temperature, T_∞ .

$$\Delta A = \pi D t - 2 \left(\pi D^2 \right) / 4$$

ΔA communicates the adjustment in the surface zone of a balance with thickness t because of entering a vertical gap with a distance across D through it.

Abdullah H. AlEssa, ET. Al. [18] thinks the expansion of normal convection heat exchange from a level rectangular balance having rectangular openings with angle proportion of two utilizing limited component procedure. The outcomes for pricked blade have been connected with its relating strong one. For geometrical measurements and warm assets of a blade and the openings one ought to do a parametric study. The study surveys the addition in blade region and of warmth exchange coefficients in light of holes. It was found that, for certain decision of rectangular measurement and spaces between holes, there is an enlargement in warmth intemperance and a lessening in weight over that of the comparing strong one. Likewise, the warmth exchange elevating of the punctured blade upsurges with the expansion in balance thickness and warm conductivity. The punctured blade results are connected with strong one to discover the expansion in warmth exchange brought on by embedding the holes. It is expected that both balances have the same sizes (the balance length is $L=50$ mm and its width is $W=200$ mm), same warm conductivity, same base temperature ($T_b=100^\circ\text{C}$) and same encompassing temperature ($T_\infty=20^\circ\text{C}$).

The study mirrored the addition in blade territory and of warmth exchange coefficients because of punctures. The outcomes uncovered that, for specific estimations of rectangular aperture measurement, the holes lead to an expansion in warmth excessiveness of the punctured blade over that of the reporter strong one. The size of warmth liberality upgrade relies on the balance thickness, its warm conductivity, and the aperture measurement, horizontal and longitudinal dividing. At last, the study uncovered that, the punctures presented in the blade supports rate of warmth decline and in the meantime decreases the heaviness of the balance.

3. CONCLUSION

If we see the overall spread of the above literature survey, it is clearly observed that the whole study is limited to the certain parameters like fin with perforation, fin without perforation, fin orientation, fin length, fin height, base to ambient temperature difference, % of perforation etc. But in the study of heat transfer heat capacity of the materials also play an important role. So there is wide scope of study w.r.t this parameter.

We will brought forward the above study –

- By comparing the results of two different materials with and without perforation **by keeping the heat capacity of both materials constant** and accordingly other properties can be varied.
- Also we can develop a **prediction model** for the values of heat transfer coefficient by using **Neural Networks (MATLAB)**.
- The above two objectives can be achieved **with constant spacing at optimum level** as mentioned in the above literature.
- The present work is primarily for **rectangular fin and fin array**. It may be further extended for **other types of fin profiles** wherever necessary.
- Maximum work is done on **tall fin** which are generally used for experimental purpose only. Actual **application based short fin** are still require more development.

REFERENCES

- [01] Starner K.E. and McManus H.N., "An Experimental Investigation of Free Convection Heat Transfer from Rectangular Fin Arrays", Journal of Heat Transfer, 273-278, (1963)
- [02] Leung C.W. and Probert S.D., "Thermal Effectiveness of Short-Protrusion Rectangular, Heat-Exchanger Fins", Applied Energy, 1-8, (1989)
- [03] Leung C.W., et al., "Heat Exchanger: Optimal Separation for Vertical Rectangular Fins Protruding from a Vertical Rectangular Base", Applied Energy, 77-85, (1985)
- [04] Welling J.R. and Wooldridge C.N., "Free Convection Heat Transfer Coefficients from Vertical Fins", Journal of Heat Transfer, 439-444, (1965)
- [05] Harahap F. and McManus H.N., "Natural Convection Heat Transfer from Horizontal Rectangular Fin Arrays", Journal of Heat Transfer, 32-38, (1967)
- [06] Jones C.D. and Smith L.F., "Optimum Arrangement of Rectangular Fins on Horizontal Surfaces for Free Convection Heat Transfer", Journal of Heat Transfer, 6-10, (1970)
- [07] Bar-Cohen A., "Fin Thickness for an Optimized Natural Convection Array of Rectangular Fins", Journal of Heat Transfer, 564-566, (1979)
- [08] Leung C.W., et al., "Heat Exchanger Design: Thermal Performances of Rectangular Fins Protruding from Vertical or Horizontal Rectangular Bases", Applied Energy, 123-140, (1985)
- [09] Leung C.W. and Probert S.D., "Heat-Exchanger Design: Optimal Uniform Thickness of Vertical Rectangular Fins Protruding Perpendicularly Outwards, at Uniform

- Separations, from a Vertical Rectangular 'Base'", Applied Energy, 111-118, (1987)*
- [10] Yüncü H. and Anbar G., "An Experimental Investigation on Performance of Rectangular Fins on a Horizontal Base in Free Convection Heat Transfer", Heat and Mass Transfer, 507-514, (1998)
- [11] Yüncü H. and Güvenc A., "An Experimental Investigation on Performance of Rectangular Fins on a Vertical Base in Free Convection Heat Transfer", Heat and Mass Transfer, 409-416, (2001)
- [12] Yüncü H. and Mobedi M., "A Three Dimensional Numerical Study on Natural Convection Heat Transfer from Short Horizontal Rectangular Fin Array", Heat and Mass Transfer, (2003)
- [13] Yüncü H. and Yıldız Ş., "An Experimental Investigation on Performance of Annular Fins on a Horizontal Cylinder in Free Convection Heat Transfer", Heat and Mass Transfer, 239-251, (2004)
- [14] Guei-Jang Huang et al., "Enhancement of natural convection heat transfer from horizontal rectangular fin arrays with perforations in fin base", Int. Journal of Thermal Sciences, 84(2014) 164-174.
- [15] Rigan Jain and M.M.Sahu., "Comparative Study of performances of Trapezoidal and Rectangular fins on a Vertical base under free convection heat transfer" IJERT vol.2 (2013) 261-272.
- [16] Yazicioğlu B., "Performance of Rectangular Fins on a Vertical Base in Free Convection Heat Transfer", M.S. Thesis in Mechanical Engineering, Middle East Technical University, Ankara (2005).
- [17] Mohamad I. Al-Widyan, Amjad Al-Shaarawi, "Numerical Investigation of Heat Transfer Enhancement for a Perforated Fin in Natural Convection" IJERA, Vol. 2, Issue 1, Jan-Feb 2012, pp.175-184.
- [18] Abdullah H. AlEssa et.al. "Enhancement of natural convection heat transfer from a fin by rectangular perforations with aspect ratio of two" International Journal of Physical Sciences Vol. 4 (10), pp. 540-547, October, 2009
- [19] Kakaç S., *Convective Heat Transfer*, METU, Ankara, (1980)
- [20] Incropera F.P. and DeWitt D.P., *Fundamentals of Heat and Mass Transfer*, John Wiley & Sons, New York, (1990)
- [21] McAdams W. H., *Heat Transmission*, McGraw-Hill, New York, (1954)
- [22] Bejan A., *Convection Heat Transfer*, John Wiley & Sons, New York, (1984)